

# Convection

- If luminosity is transported by radiation, then it must obey

$$L_r = -\frac{16\pi a c r^2 T^3}{3\rho\kappa_R} \frac{dT}{dr}$$

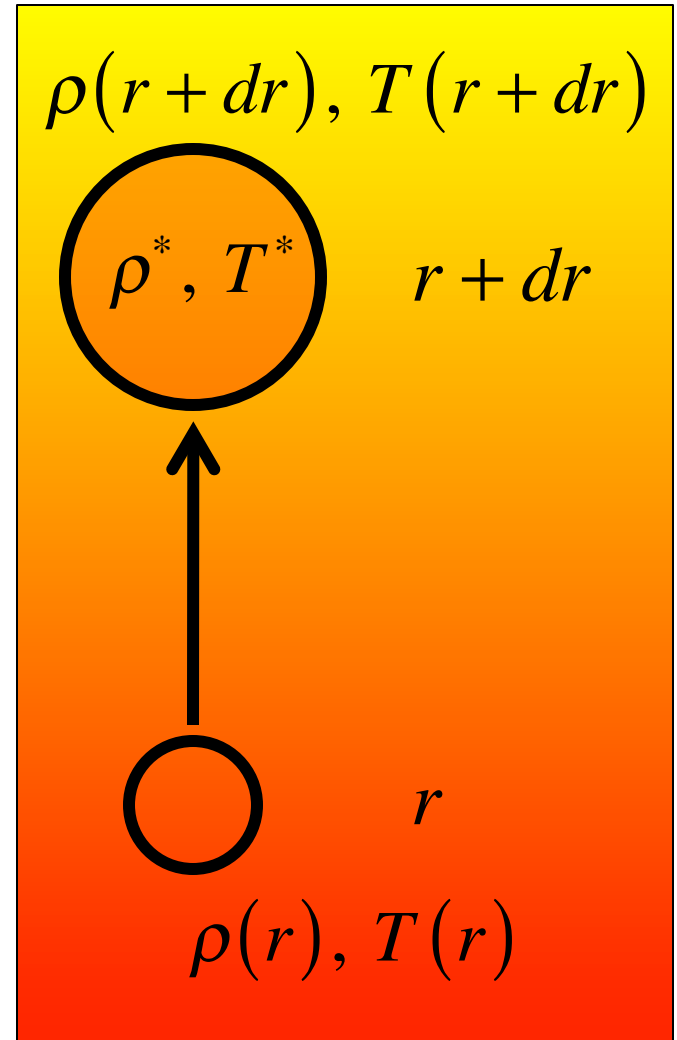
- In a steady state, the energy transported per time at radius  $r$  must be equal to the energy generation rate in the stellar interior.

$$\rightarrow \frac{dT}{dr} \text{ will be large if } \begin{cases} L \text{ is large} \\ \kappa_R \text{ is large} \end{cases}$$

- The temperature gradient cannot be arbitrarily large. If it gets too steep  $\rightarrow$  convection takes over as the main mode of energy transport.

# Convection: Stability Criteria

- Uniform composition,  $T(r)$ ,  $\rho(r)$  profiles
- Displace a mass element by  $dr$  without exchanging heat with the environment (adiabatically).
- Element expands to maintain pressure balance with its environment.
- Its new density  $\rho^*$  and temperature  $T^*$  will not in general equal the ambient values at  $r + dr$ .



# Convection: Stability Criteria

- Since the change is adiabatic:

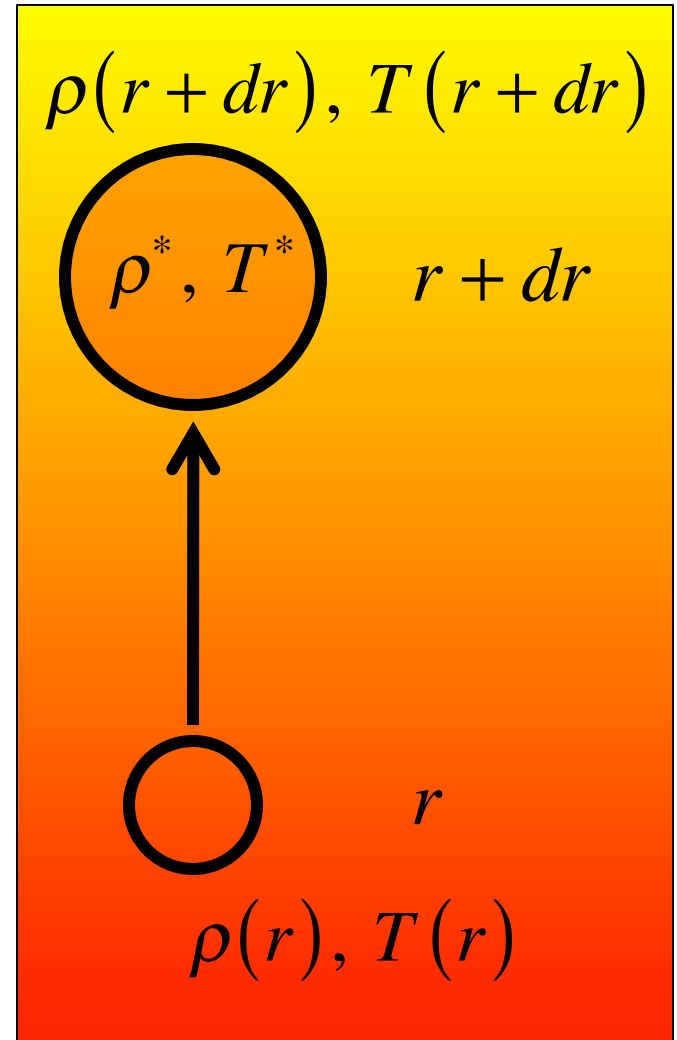
$$\left( \frac{d \ln P}{d \ln \rho} \right)_{\text{ad}} = \Gamma_1 \quad \rightarrow \quad \frac{\rho}{P} \left( \frac{dP}{d\rho} \right)_{\text{ad}} = \Gamma_1$$

$$\rightarrow (d\rho)_{\text{ad}} = \frac{\rho}{\Gamma_1 P} (dP)_{\text{ad}}$$

$$\rho^* = \rho(r) + (d\rho)_{\text{ad}} = \rho(r) + \frac{\rho}{\Gamma_1 P} (dP)_{\text{ad}}$$

$$= \rho(r) + \frac{\rho}{\Gamma_1 P} \left( \frac{dP}{dr} \right)_{\text{ad}} dr$$

- Since pressure equilibrium applies:  $\left( \frac{dP}{dr} \right)_{\text{ad}} = \frac{dP}{dr}$



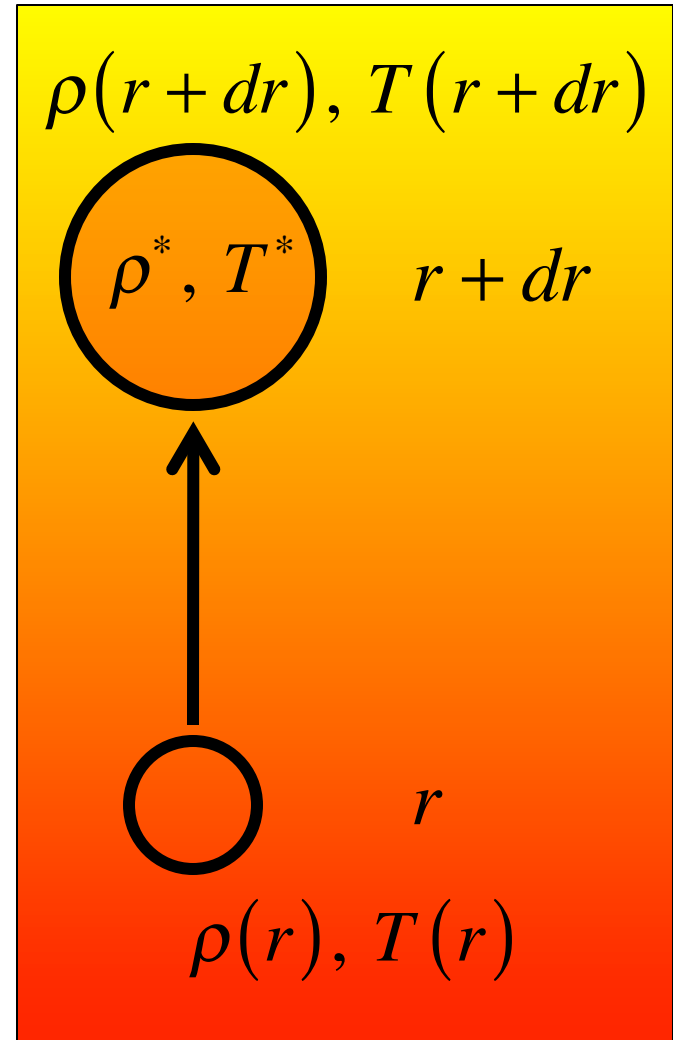
# Convection: Stability Criteria

- If  $\rho^* > \rho(r + dr)$  : displaced element will be denser than its surroundings and will settle back down  $\rightarrow$  **STABILITY**
- If  $\rho^* < \rho(r + dr)$  : buoyancy will cause element to rise further  $\rightarrow$  **INSTABILITY**
- Stability criterion is:

$$\rho(r) + \frac{\rho}{\Gamma_1 P} \frac{dP}{dr} dr > \rho(r + dr)$$

$$\rightarrow \frac{\rho(r + dr) - \rho(r)}{dr} < \frac{\rho}{\Gamma_1 P} \frac{dP}{dr}$$

$$\boxed{\frac{d\rho}{dr} < \frac{\rho}{\Gamma_1 P} \frac{dP}{dr}}$$



# Convection: Stability Criteria

- Since the change is adiabatic:

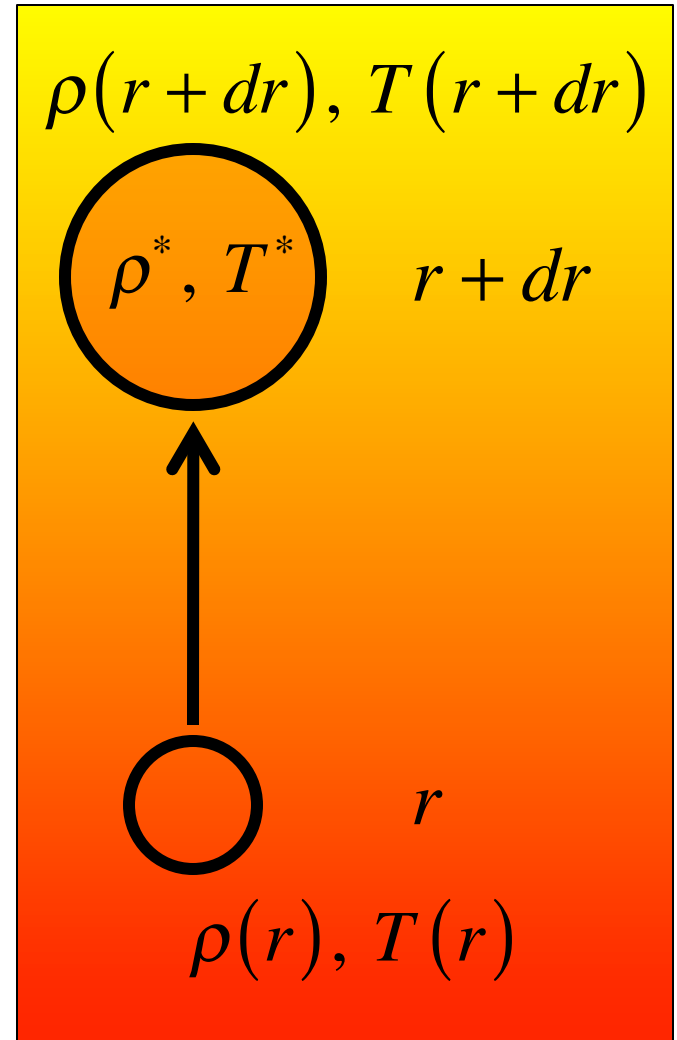
$$\left(\frac{d \ln P}{d \ln T}\right)_{\text{ad}} = \frac{\Gamma_2}{\Gamma_2 - 1} \rightarrow \frac{T}{P} \left(\frac{dP}{dT}\right)_{\text{ad}} = \frac{\Gamma_2}{\Gamma_2 - 1}$$

$$\rightarrow (dT)_{\text{ad}} = \frac{\Gamma_2 - 1}{\Gamma_2} \frac{T}{P} (dP)_{\text{ad}}$$

$$T^* = T(r) + (dT)_{\text{ad}}$$

$$= T(r) + \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} (dP)_{\text{ad}}$$

$$= T(r) + \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr} dr$$



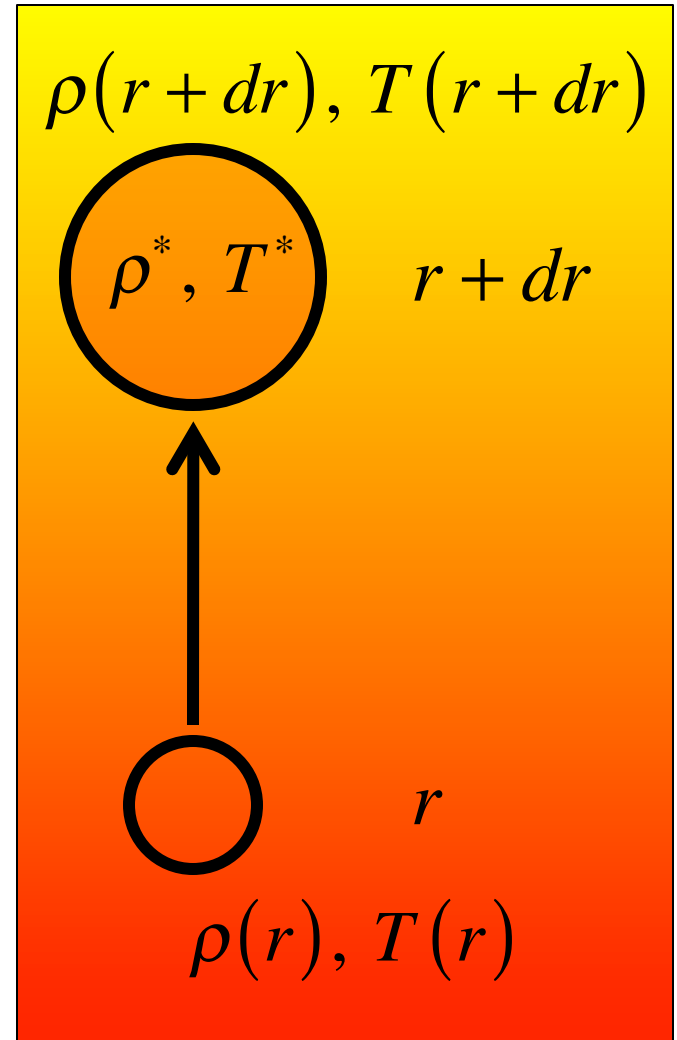
# Convection: Stability Criteria

- If  $T^* < T(r + dr)$  : displaced element will be cooler than its surroundings and will settle back down → **STABILITY**
- If  $T^* > T(r + dr)$  : element will be hotter and thus rise → **INSTABILITY**
- Stability criterion is:

$$T(r) + \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr} dr < T(r + dr)$$

$$\rightarrow \frac{T(r + dr) - T(r)}{dr} > \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr}$$

$$\frac{dT}{dr} > \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr}$$

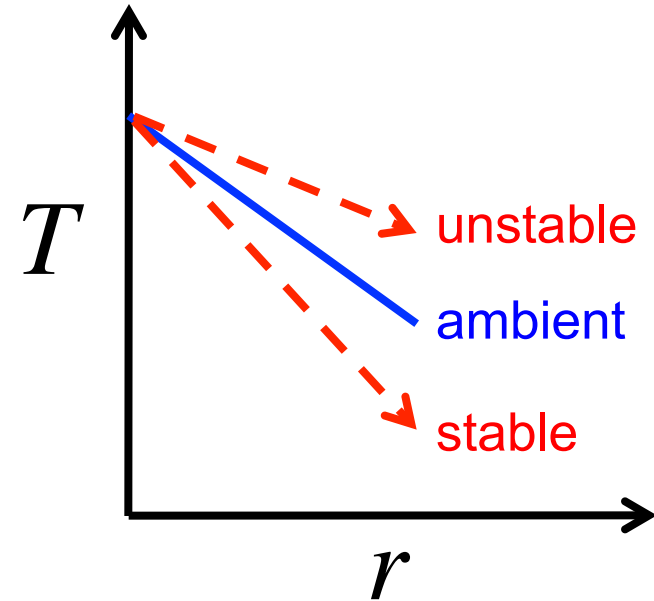


# Convection: Stability Criteria

- Stability criterion is:

$$\frac{dT}{dr} > \left( \frac{dT}{dr} \right)_{\text{ad}}$$

$$\left| \frac{dT}{dr} \right| < \left| \left( \frac{dT}{dr} \right)_{\text{ad}} \right|$$



- Too rapid a change in temperature  $\rightarrow$  CONVECTION

$$\frac{dT}{dr} < \left( 1 - \frac{1}{\Gamma_2} \right) \frac{T}{P} \frac{dP}{dr}$$

# Convection: Stability Criteria

- Convert to maximum luminosity that can be carried by radiation

$$\frac{dT}{dr} = -\frac{3\rho\kappa_R L_r}{16\pi a c r^2 T^3} > \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr}$$

$$\frac{3\rho\kappa_R L_r}{16\pi a c r^2 T^3} < -\left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr}$$

$$\frac{dP}{dr} = -\rho \frac{Gm}{r^2}$$

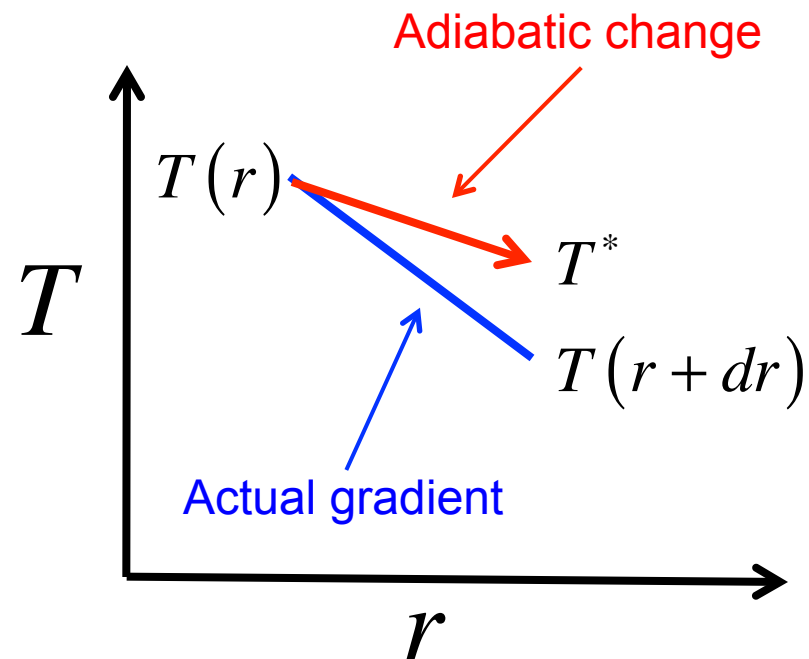
$$L_r < \frac{16\pi a c G}{3\kappa_R} \left(1 - \frac{1}{\Gamma_2}\right) \frac{T^4 m}{P}$$

- If L exceeds this value → CONVECTION



# Convection: Stability Criteria

- In an unstable region, displaced element is hotter than ambient gas  
→ continues to rise
- Eventually, radiation will leak out of the rising gas element.  
→ extra energy flux from hotter to cooler regions



- What causes convective instability in some regions of a star?

$$L_{\max} \sim \frac{1}{\kappa_R} \left( 1 - \frac{1}{\Gamma_2} \right) \frac{T^4 m}{P}$$

When  $L_{\max}$  is low → convection

# Convection: Stability Criteria

Near surface

$$m \approx M$$

$$\frac{T^4}{P} \approx \text{const}$$

$$L_{\max} \sim \frac{1}{\kappa_R} \left( 1 - \frac{1}{\Gamma_2} \right) \frac{T^4 m}{P}$$

$$L_{\max} \sim \frac{1}{\kappa_R} \left( 1 - \frac{1}{\Gamma_2} \right)$$

Remember

$$\Gamma_2 = 5/3$$

Vulnerable to convection if

$\kappa_R$  is large

Occurs when there is a large contribution from atomic processes.

$\Gamma_2 \rightarrow 1$

Occurs in ionization zones where  $\Gamma_2$  dips below 4/3

So, atomic processes + ionization zones  $\rightarrow$  convection will happen  
In regions where  $T \sim 10^4 - 10^5 \text{K}$  and  $H$  is being ionized.

Not in high mass stars

# Convection: Stability Criteria

Near center

$\kappa_R$  is low

$\Gamma_2$  is high

$$L_{\max} \sim \frac{1}{\kappa_R} \left( 1 - \frac{1}{\Gamma_2} \right) \frac{T^4 m}{P}$$

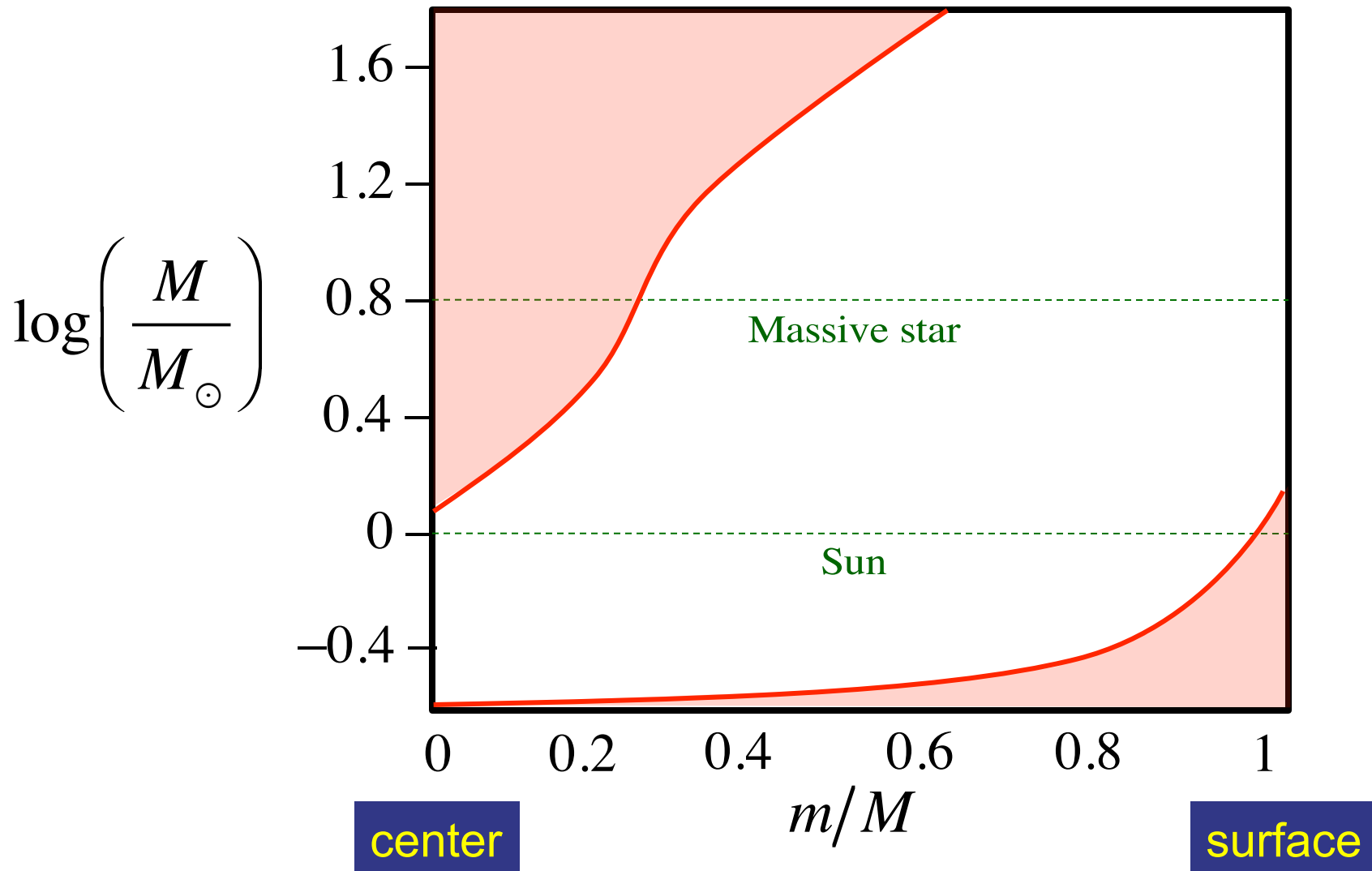
$$L_{\max} \sim m$$

Vulnerable to convection if there is a large luminosity at low mass.

This happens when nuclear energy generation is a very strong function of  $T$ . CNO in massive stars.

# Convection

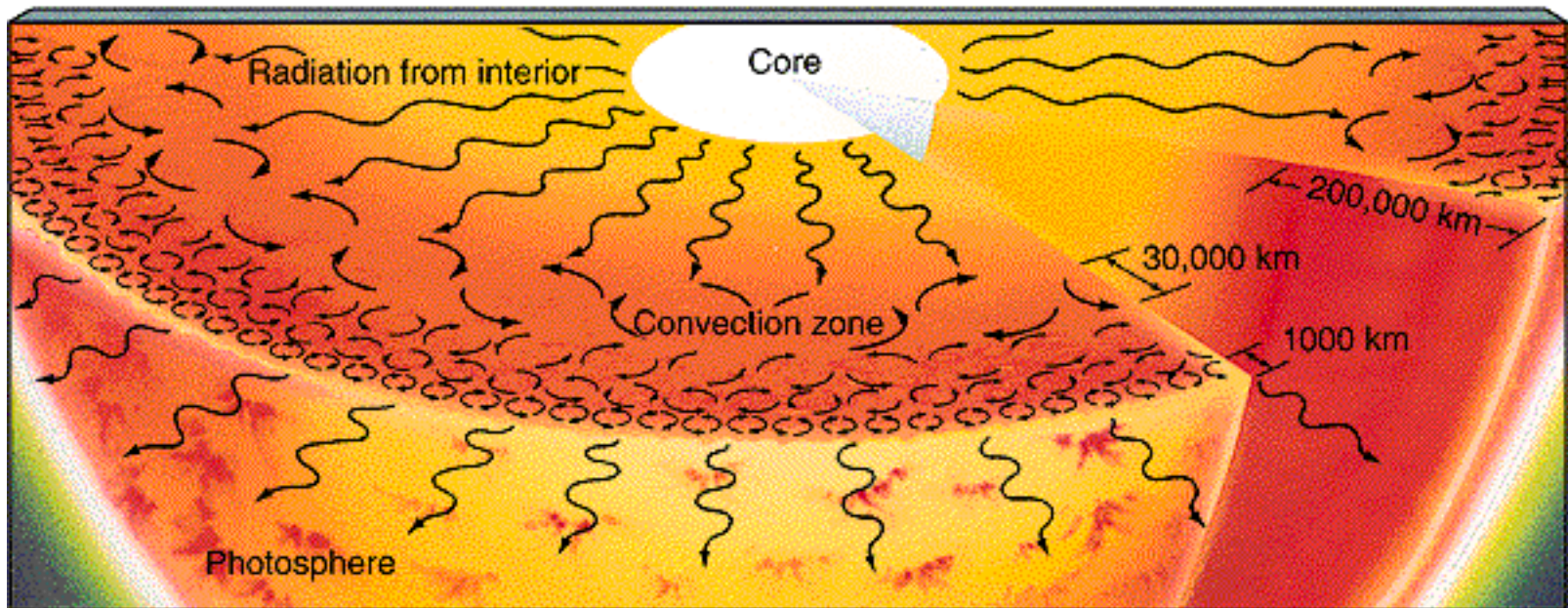
Zero-age main sequence stars



# Convection

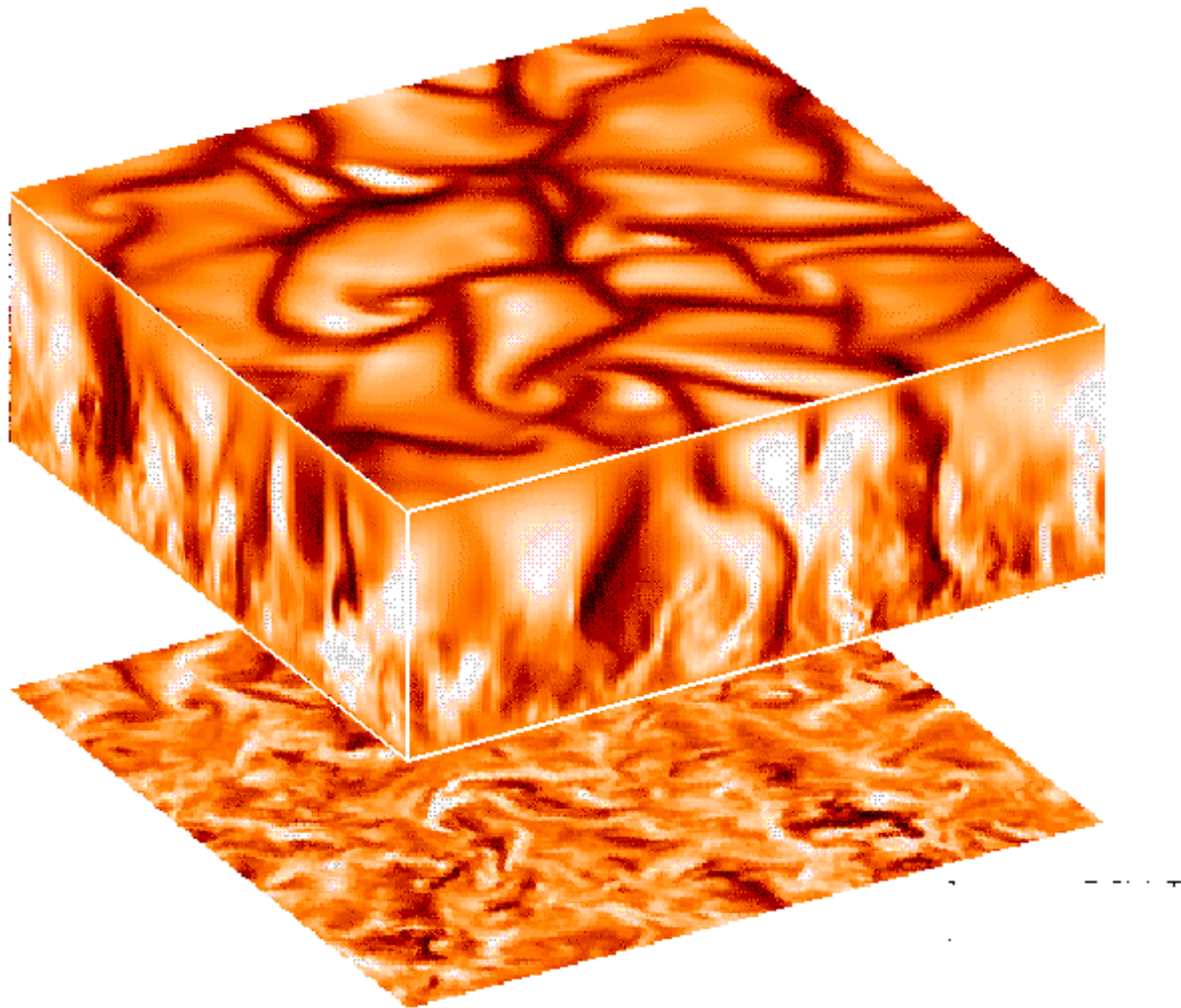
Very low mass Main sequence	Fully convective
Low mass Main sequence	Radiative core Convective surface
High mass Main sequence	Convective core Radiative surface
White dwarfs	Conductive

# Convection



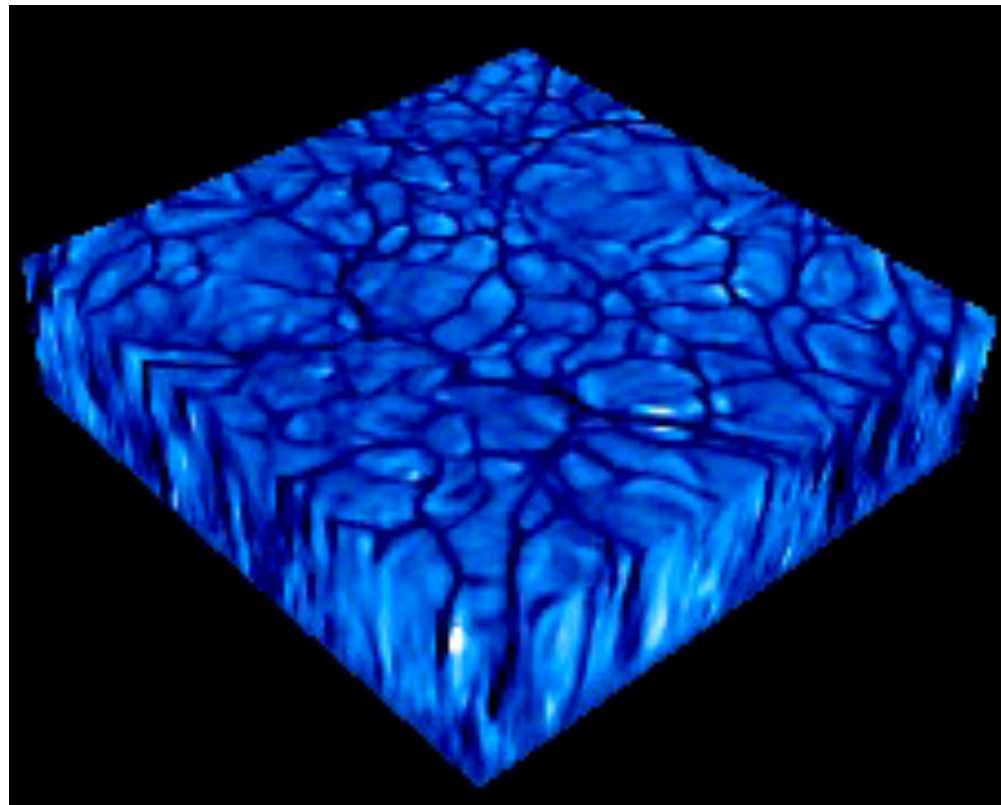
# Convection

Convection is incredibly difficult to model accurately because fluid motions are very complicated. It is a 3D problem.



# Convection

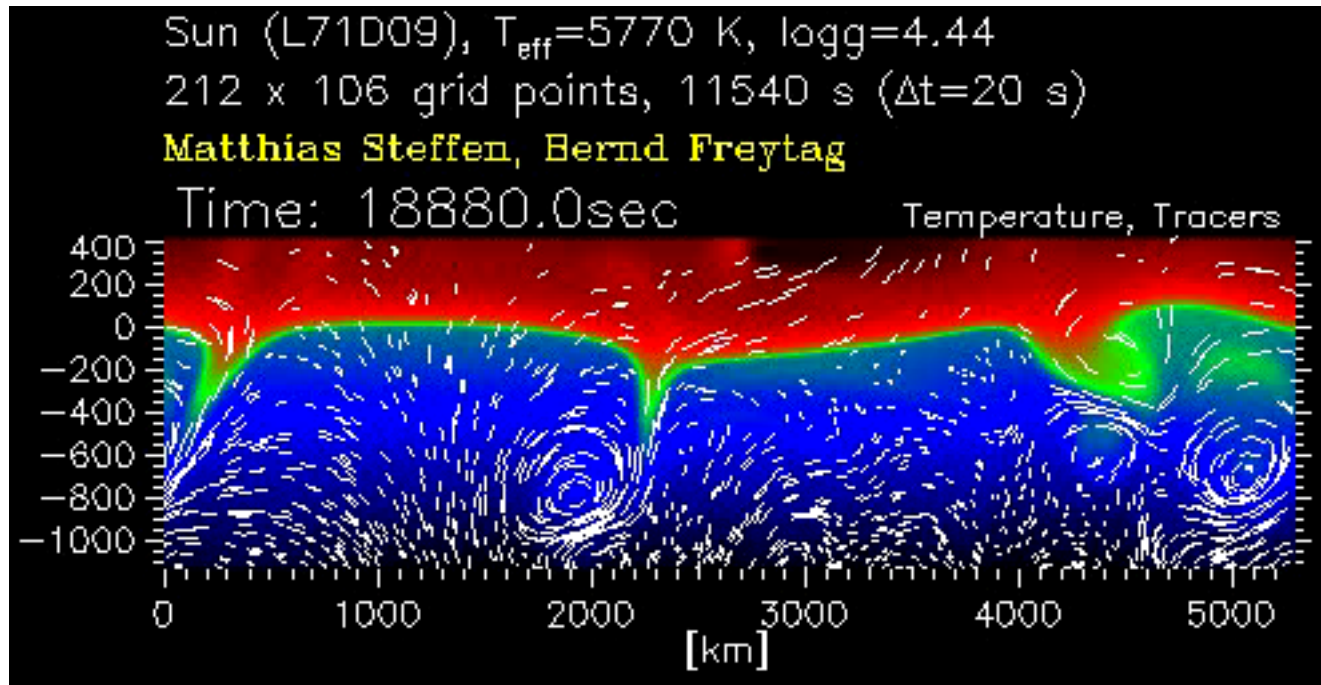
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# Convection

Convection is incredibly difficult to model accurately because fluid motions are very complicated. It is a 3D problem.



# Convection: Energy Flux

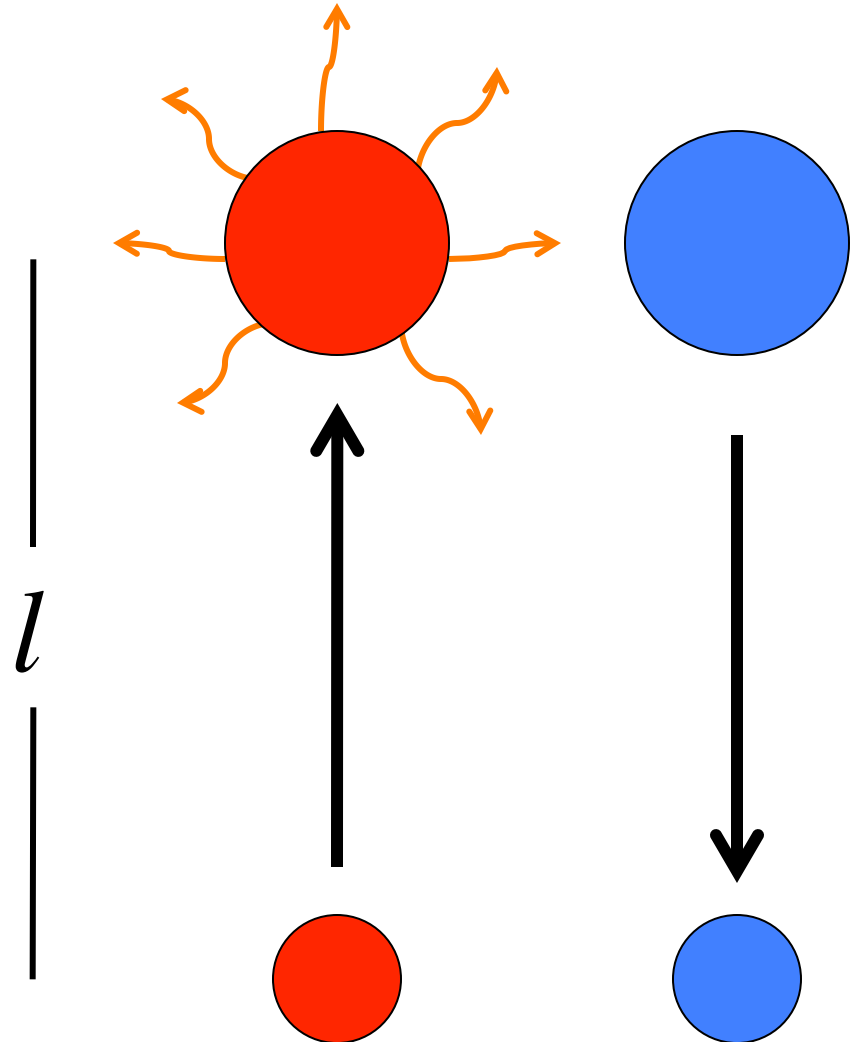
- No reliable analytic way to compute
- Lab experiments with fluids are not relevant
  - incompressible
  - too viscous
  - boundaries
- Hydrodynamic simulations are challenging
- Empirical simple model for spherically symmetric stellar models: Mixing Length Theory

# Convection: Mixing Length Theory

1 parameter: length of mixing

Each mass element  
rises or falls a distance  
 $l$  adiabatically

After one mixing length,  
The element thermalizes  
with the local environment.



# Convection: Mixing Length Theory

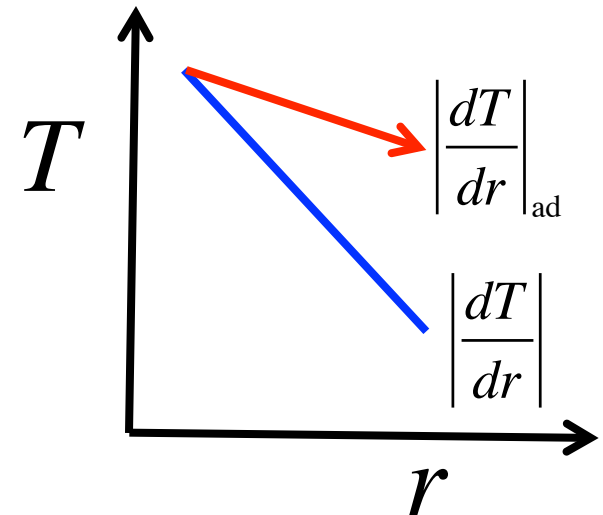
- $l$  should scale with the pressure scale height

$$\lambda_P = P \left| \frac{dP}{dr} \right|^{-1} \quad (\text{length over which pressure changes by 100\%})$$

$$l = \alpha \cdot \lambda_P \quad \alpha : \text{free parameter} \quad (\alpha = 1.6 \pm 0.1)$$

- After rising adiabatically by a distance  $l$ , the mass element will be hotter than its surrounding gas by

$$\Delta T = \left( \left| \frac{dT}{dr} \right| - \left| \frac{dT}{dr} \right|_{\text{ad}} \right) \cdot l \equiv l \cdot \Delta \nabla T$$



# Convection: Mixing Length Theory

- If the mass element thermalizes at constant pressure, the amount of heat per unit mass released is

$$\Delta Q = c_p \Delta T = c_p l \Delta \nabla T$$

- If the average velocity of the mass element is  $\bar{v}$ , the average excess heat flux is

$$F_{\text{conv}} = \rho \bar{v} \Delta Q = \rho \bar{v} c_p l \Delta \nabla T$$

$$\frac{\text{heat}}{\text{mass}} \times \frac{\text{mass}}{\text{volume}} \times \frac{\text{length}}{\text{time}} = \frac{\text{heat}}{\text{area} \cdot \text{time}}$$

- The mass element is accelerated due to buoyancy ( $\rho < \rho_{\text{ambient}}$ )

$$\Delta \rho = \left( \left| \frac{d\rho}{dr} \right| - \left| \frac{d\rho}{dr} \right|_{\text{ad}} \right) l \equiv l \Delta \nabla \rho \quad \rightarrow \quad \overline{\Delta \rho} = \frac{1}{2} l \Delta \nabla \rho$$

# Convection: Mixing Length Theory

- The average buoyant force per unit volume is

$$\bar{F} = g \cdot \overline{\Delta\rho} = \frac{1}{2} gl \Delta\nabla\rho \quad \text{where } g = \frac{Gm}{r^2}$$

- The resulting acceleration is

$$\bar{a} = \frac{\bar{F}}{\rho} = \frac{gl}{2\rho} \Delta\nabla\rho = \frac{Gml}{2\rho r^2} \Delta\nabla\rho$$

- If the mass element starts at rest and has a constant acceleration

$$\left. \begin{aligned} v &= \bar{a} \cdot t \\ t &= \frac{l}{\bar{v}} = \frac{l}{\frac{1}{2}v} = \frac{2l}{v} \end{aligned} \right\} \rightarrow v = (2\bar{a}l)^{1/2} \rightarrow \bar{v} = \frac{1}{2}(2\bar{a}l)^{1/2}$$
$$\rightarrow \bar{v} = \frac{l}{2} \left( \frac{Gm}{\rho r^2} \Delta\nabla\rho \right)^{1/2}$$

# Convection: Mixing Length Theory

$$F_{\text{conv}} = \rho \bar{v} c_p l \Delta \nabla T$$

$$\bar{v} = \frac{l}{2} \left( \frac{Gm}{\rho r^2} \Delta \nabla \rho \right)^{1/2}$$

$$F_{\text{conv}} = \frac{l}{2} \left( \frac{Gm}{\rho r^2} \Delta \nabla \rho \right)^{1/2} \rho c_p l \Delta \nabla T$$

$$\Delta \nabla \rho \equiv \left( \left| \frac{d\rho}{dr} \right| - \left| \frac{d\rho}{dr} \right|_{\text{ad}} \right) \approx \frac{\rho}{T} \left( \left| \frac{dT}{dr} \right| - \left| \frac{dT}{dr} \right|_{\text{ad}} \right) \equiv \frac{\rho}{T} \Delta \nabla T$$

$$F_{\text{conv}} = \frac{l}{2} \left( \frac{Gm}{\rho r^2} \frac{\rho}{T} \Delta \nabla T \right)^{1/2} \rho c_p l \Delta \nabla T$$

$$F_{\text{conv}} = \frac{l^2}{2} c_p \rho \left( \frac{Gm}{Tr^2} \right)^{1/2} (\Delta \nabla T)^{3/2}$$

# Convection: Mixing Length Theory

- How large an excess T gradient is needed to carry luminosity?

$$(\Delta \nabla T)^{3/2} = \frac{\frac{L_r}{4\pi r^2}}{\frac{l^2}{2} c_P \rho \left( \frac{Gm}{Tr^2} \right)^{1/2}} = \frac{L_r}{2\pi l^2 c_P \rho r (Gm/T)^{1/2}}$$

e.g., at  $\frac{m}{M} = 0.5$ ,  $l = \lambda_p = 5 \times 10^9$  cm, solar values for  $T, \rho, r, L_r, c_P$

$$\Delta \nabla T \sim 10^{-10} \text{ Kcm}^{-1} \quad \left| \frac{dT}{dr} \right| \approx \frac{T_c}{R} \sim 10^{-4} \text{ Kcm}^{-1}$$

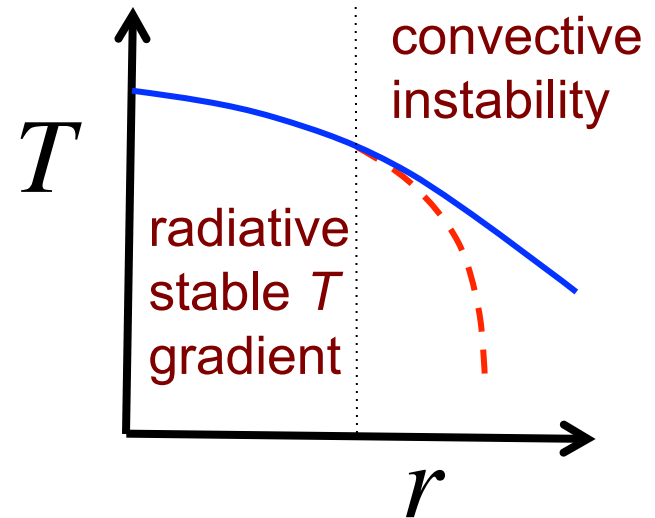
Requires an excess of only  $\sim 10^{-6}$  of the temperature gradient!



# Convection: Mixing Length Theory

- When convection occurs in stellar interiors, the resulting temperature gradient equals the adiabatic gradient.

$$\frac{dT}{dr} = \left( \frac{dT}{dr} \right)_{\text{ad}} + \cancel{\Delta \nabla T}$$
$$\approx \left( 1 - \frac{1}{\Gamma_2} \right) \frac{T}{P} \frac{dP}{dT}$$



- If composition changes with radius, this may be different. e.g., if  $\mu$  drops with  $r \rightarrow$  heavier material is displaced into lighter material  $\rightarrow$  greater stability.

Nuclear burning  $\rightarrow$  stabilizing

# Convection: Mixing Length Theory

- When convection is efficient, the exact value of the mixing length  $l$  does not matter.

Near surface,  $\lambda_p$  is small  $\rightarrow$  larger  $\Delta\nabla T$  is needed.

- Stellar radius  $R$ , surface  $T$ , etc. depend on  $\alpha$

x2 change in  $\alpha$   $\rightarrow$  few hundred K difference in  $T_{\text{eff}}$ .

# Convection: Mixing Length Theory

## Convective Overshooting

Do convective elements overshoot into stable regions due to inertia?

Naively: No because acceleration is small and braking is large in stable zone.

Simulations: Overshooting extends to significant fraction of  $\lambda_P$

## Alternative to Mixing Length model

“Full spectrum of turbulence”

Turbulent processes involve a range of length scales.

It is unclear if this works better than the one-parameter model.

