

Summary of Results

1. Mass Conservation

$$\frac{dm}{dr} = 4\pi r^2 \rho$$

eulerian

$$\frac{dr}{dm} = \frac{1}{4\pi r^2 \rho}$$

lagrangian

Summary of Results

2. Hydrostatic Equilibrium

$$\frac{dP}{dr} = -\rho \frac{Gm}{r^2}$$

eulerian

$$\frac{dP}{dm} = -\frac{Gm}{4\pi r^4}$$

lagrangian

Need equation of state: $P = f(\rho, T, X_i)$

Summary of Results

3. Energy Generation

$$\frac{dL_r}{dr} = 4\pi r^2 \rho \varepsilon$$

eulerian

$$\frac{dL_m}{dm} = \varepsilon$$

lagrangian

Need nuclear physics:

$$\varepsilon = f(\rho, T, X_i)$$

Summary of Results

4. Energy Flow: Radiation

$$\frac{dT}{dr} = - \frac{3\kappa\rho L_r}{16\pi a c r^2 T^3}$$

eulerian

$$\frac{dT}{dm} = - \frac{3\kappa L_m}{64\pi^2 a c r^4 T^3}$$

lagrangian

Need opacity: $\kappa = f(\rho, T, X_i)$

Summary of Results

4. Energy Flow: Convection

$$\frac{dT}{dr} = - \left(1 - \frac{1}{\Gamma_2} \right) \frac{Gm\rho T}{r^2 P}$$

eulerian

$$\frac{dT}{dm} = - \left(1 - \frac{1}{\Gamma_2} \right) \frac{GmT}{4\pi r^4 P}$$

lagrangian

Need adiabatic exponent: $\Gamma_2 = f(\rho, T, X_i)$

Summary of Results

Equation of State (non-degenerate matter)

$$P = \frac{1}{3} a T^4 + \frac{N_A k}{\mu} \rho T$$

Mean molecular weight: $\frac{1}{\mu} = \frac{1}{\mu_i} + \frac{1}{\mu_e} = \sum_i \frac{X_i}{A_i} + \sum_i \frac{Z_i X_i y_i}{A_i}$

Summary of Results

Ionization fractions y_i

Saha equation :

$$\frac{n^+ n_e}{n^0} = \frac{2G^+}{G^0} \frac{(2\pi m_e kT)^{3/2}}{h^3} \exp\left(-\frac{\chi}{kT}\right)$$

e.g., Hydrogen only :

$$\frac{y^2}{1-y} = \frac{1}{N_A \rho} \frac{(2\pi m_e kT)^{3/2}}{h^3} \exp\left(-\frac{\chi_H}{kT}\right)$$

Summary of Results

Thermodynamics

Adiabatic index :

$$\frac{\Gamma_2}{\Gamma_2 - 1} = \left(\frac{\partial \ln P}{\partial \ln T} \right)_{ad}$$

$$\Gamma_2 = \frac{32 - 24\beta - 3\beta^2}{24 - 18\beta - 3\beta^2} \quad \beta = \frac{P_g}{P_{tot}}$$

(assuming neutral or fully ionized gas)

Summary of Results

Opacity: approximations

$$\frac{1}{\kappa} \approx \frac{1}{\kappa_{H^-}} + \frac{1}{\kappa_e + \kappa_{ff} + \kappa_{bf}}$$

$$\kappa_e = 0.2(1 + X) \text{cm}^2 \text{g}^{-1} \quad (\text{assuming fully ionized and no metals})$$

$$\kappa_{ff} \approx 4 \times 10^{22} (X + Y)(1 + X) \rho T^{-3.5} \text{cm}^2 \text{g}^{-1}$$

$$\kappa_{bf} \approx 4 \times 10^{25} Z(1 + X) \rho T^{-3.5} \text{cm}^2 \text{g}^{-1}$$

$$\kappa_{H^-} \approx 2.5 \times 10^{-31} (Z/0.02) \rho^{1/2} T^9 \text{cm}^2 \text{g}^{-1}$$

Summary of Results

Opacity: tables

Interpolate in density,
temperature, and
composition.

$\log T = 6.192$

$\log R$	-6.0	-5.5
$\log T$		
6.1	-0.429	-0.409
6.2	-0.429	-0.397

$\log R = -5.83$



Summary of Results

Convection

Convection happens when:

$$\left| \frac{dT}{dr} \right|_{rad} > \left| \frac{dT}{dr} \right|_{ad}$$

$$L_m > \frac{16\pi acG}{3\kappa_R} \left(1 - \frac{1}{\Gamma_2} \right) \frac{T^4 m}{P}$$

Summary of Results

Energy generation

$$\varepsilon = \varepsilon_{pp} + \varepsilon_{CNO} + \varepsilon_{3\alpha}$$

$$\varepsilon_{pp} = 2.4 \times 10^4 \frac{\rho X^2}{T_9^{2/3}} \exp(-3.38/T_9^{1/3}) \text{ergs}^{-1} \text{g}^{-1}$$

$$\varepsilon_{CNO} \approx 4.4 \times 10^{25} \frac{\rho XZ}{T_9^{2/3}} \exp(-15.228/T_9^{1/3}) \text{ergs}^{-1} \text{g}^{-1}$$

$$\varepsilon_{3\alpha} = 5 \times 10^8 \frac{\rho^2 Y^3}{T_9^3} \exp(-4.4/T_9) \text{ergs}^{-1} \text{g}^{-1}$$

Stellar Models

Given M and X, Y, Z , solve structure equations

$$\frac{dr}{dm}$$

$$\frac{dP}{dm}$$

$$\frac{dT}{dm}$$

$$\frac{dL_m}{dm}$$

to get r, P, T, L_m as a function of m

Need to know:

$$\rho(P, T, X, Y, Z)$$

$$\varepsilon(\rho, T, X, Y, Z)$$

$$\kappa_R(\rho, T, X, Y, Z)$$

$$\Gamma_2(\rho, T, X, Y, Z)$$

Stellar Models

CENTER

$$m = 0$$

$$r = 0 \quad \checkmark$$

$$P = P_c$$

$$T = T_c$$

$$L_m = 0 \quad \checkmark$$

SURFACE

$$m = M$$

$$r = R$$

$$P \approx 0 \quad \checkmark$$

$$T \approx 0 \quad \checkmark$$

$$L_m = L$$

Stellar Models

$$\frac{dr}{dm} = \frac{1}{4\pi r^2 \rho}$$

$$\frac{dP}{dm} = -\frac{Gm}{4\pi r^4}$$

$$\frac{dL_m}{dm} = \varepsilon$$

$$\frac{dT}{dm} = -\frac{3\kappa L_m}{64\pi^2 a c r^4 T^3}$$

$$\frac{dT}{dm} = -\left(1 - \frac{1}{\Gamma_2}\right) \frac{GmT}{4\pi r^4 P}$$

- Some of these equations are indeterminate at center.
- It is better to start the integration at a very small $m > 0$.

Stellar Models

Central boundary conditions

At a very small $m > 0$:

$$r \neq 0$$

$$m = \frac{4}{3} \pi r^3 \rho_c \rightarrow r = \left(\frac{3m}{4\pi\rho_c} \right)^{1/3}$$

$$L_m \neq 0$$

$$L_m = \varepsilon_c m$$

Stellar Models

Central boundary conditions

- We can get boundary conditions for P and T by expanding and demanding that their derivatives are zero at $r=0$

$$P(r) = P(0) + \cancel{P'(0)}(r-0) + \frac{1}{2}P''(0)(r-0)^2$$
$$= P_c + P''(0)\frac{r^2}{2}$$

$$P'(r) = -\frac{Gm\rho}{r^2}$$

$$= -\frac{G\rho}{r^2} \left(\frac{4}{3}\pi r^3 \rho_c \right) = -\frac{4}{3}\pi G\rho_c^2 r$$

$$P(r) = P_c - \frac{2}{3}\pi G\rho_c^2 r^2$$

Stellar Models

Central boundary conditions

- Similarly,

$$T(r) = T(0) + \cancel{T'(0)}(r-0) + \frac{1}{2}T''(0)(r-0)^2$$

$$= T_c + T''(0)\frac{r^2}{2}$$

Radiative

$$T(r) = T_c - \frac{\kappa_c \rho_c^2 \epsilon_c}{8acT_c^3} r^2$$

$$T'(r) = -\frac{3\kappa_R \rho L_r}{16\pi ac r^2 T^3}$$

Convective

$$T(r) = T_c - \left(1 - \frac{1}{\Gamma_{2,c}}\right) \frac{2\pi G \rho_c^2 T_c}{3P_c} r^2$$

$$T'(r) = \left(1 - \frac{1}{\Gamma_2}\right) \frac{T}{P} \frac{dP}{dr}$$

Stellar Models

Surface boundary conditions

- We can do better than $T=P=0$ at surface.

guess R and L:

$$L = 4\pi R^2 \sigma T_s^4 \rightarrow T_s = \left(\frac{L}{4\pi R^2 \sigma} \right)^{1/4}$$

Guess ρ very small, e.g., $10^{-5} \text{ g cm}^{-3}$:

$$P_s = \frac{1}{3} a T_s^4 + \frac{N_A k}{\mu} \rho_s T_s$$

Stellar Models

Steps in constructing a stellar model

1. Compute $\rho, \kappa, \epsilon, \Gamma_2$ as a function of P, T, X, Y, Z

DENSITY

- Beware of P dropping below

OPACITY

- Use approximations for crude results
- Interpolate using tables (use approximations outside table bounds)

$$\frac{1}{3} a T^4$$

ENERGY GENERATION

- Use formulas for pp, CNO, and 3

THERMODYNAMICS

- 5/3 for ideal gas, 4/3 for radiation pressure
- departs from these values when
 - Mixture of ideal gas and radiation
 - Ionization zones

α

$$\Gamma_2 =$$

$$\Gamma_2$$

Stellar Models

Steps in constructing a stellar model

2. Use four structure equations to compute m for these (boundary conditions) vs. given starting values r, P, T, L_m

- Given values of m, r, P, T, L_m at shell compute 4 derivatives:

- Use these derivatives to compute $m, r, P, T, L_m, \rho, \kappa, \epsilon, \Gamma_2$ at shell i

e.g.,

$$\frac{dr}{dm}, \frac{dP}{dm}, \frac{dL_m}{dm}, \frac{dT}{dm}$$

- Shell size $i + 1$ near center and surface. r, P, T, L_m

$i + 1$

$$r[i + 1] = r[i] + \left(\frac{dr}{dm} \right) [i] \times dm$$

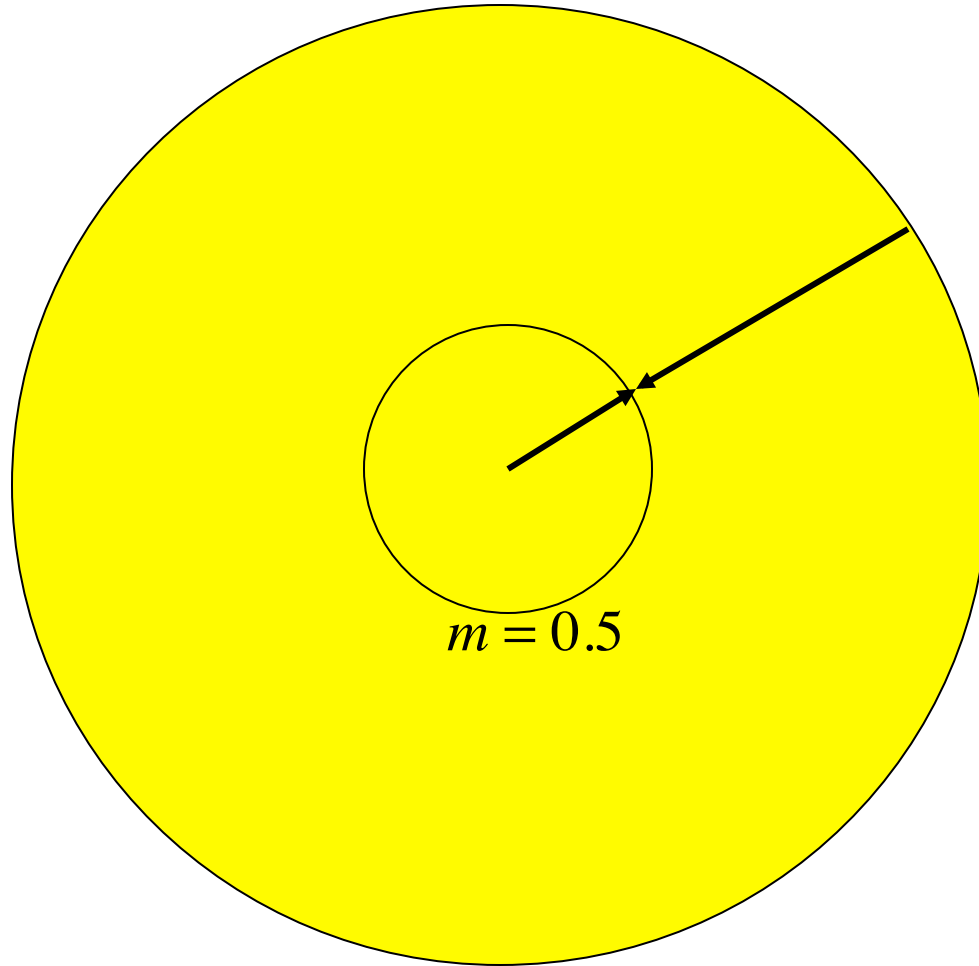
$$dm < 10^{-4} M$$

Stellar Models

Steps in constructing a stellar model

3. Deal with lack of complete boundary conditions at center or surface.
 - At center, have r , L_m , but not P , T
 - At surface, have P , T , but not r , L_m
 - General approach: guess values for missing conditions at one end, run model, and compare boundary conditions at other end.
PROBLEM: small changes in conditions at center can cause large differences at surface → difficult to reach convergence.
SOLUTION: Shoot from both center and surface and meet halfway through star.

Stellar Models

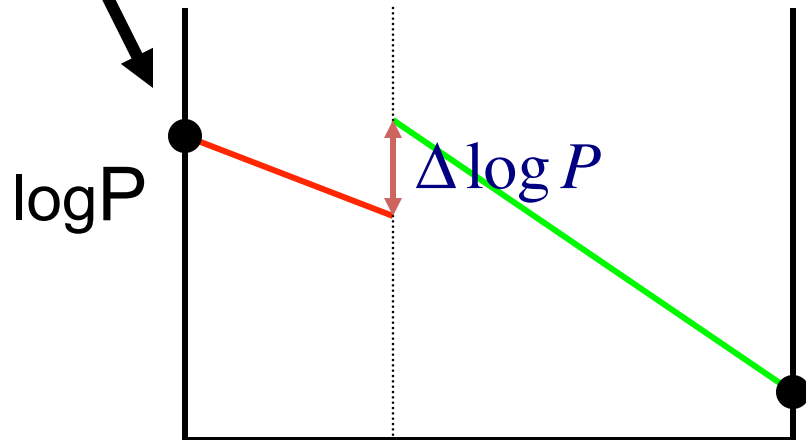


Stellar Models

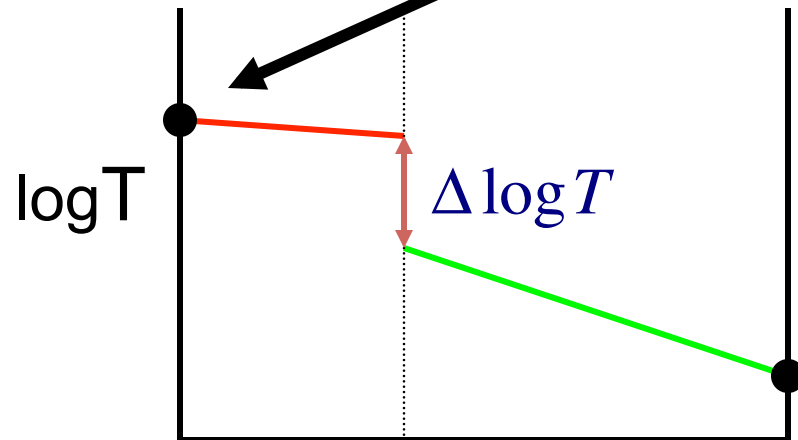
- Guess values for T_c and P_c and integrate outwards from $m = 0$ to $m = M/2$
- Guess values for R and L and integrate inwards from $m = M$ to $m = M/2$
- Compute discrepancies $\Delta r, \Delta P, \Delta T, \Delta L_m$ at $m = M/2$
- Work in log space: $\log P, \log T, \log r, \log L_m$

Stellar Models

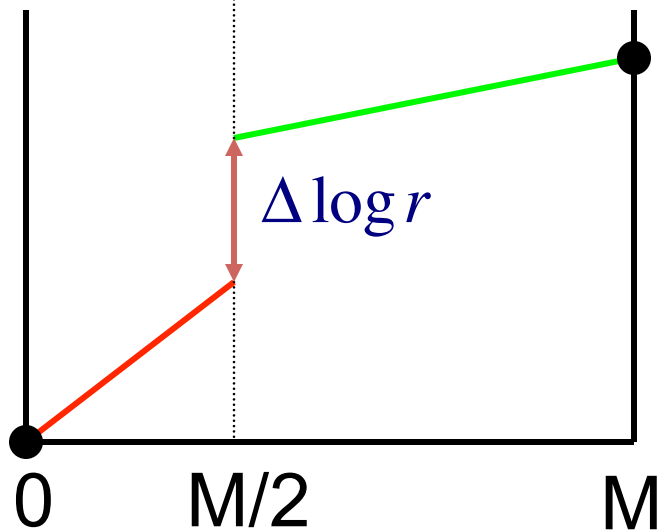
guess



guess

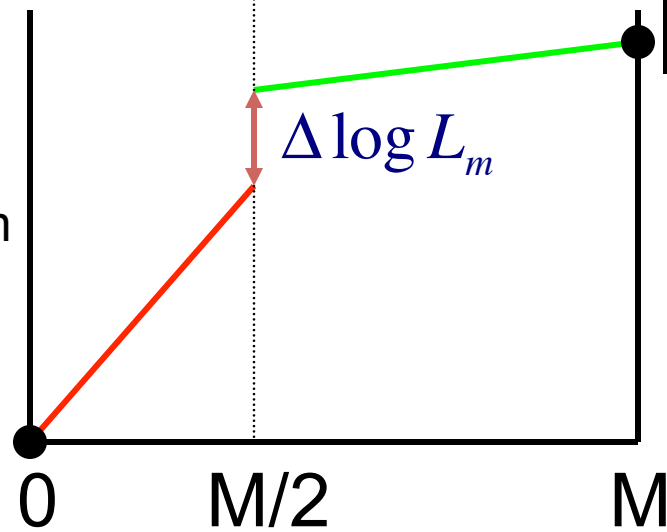


$\log r$



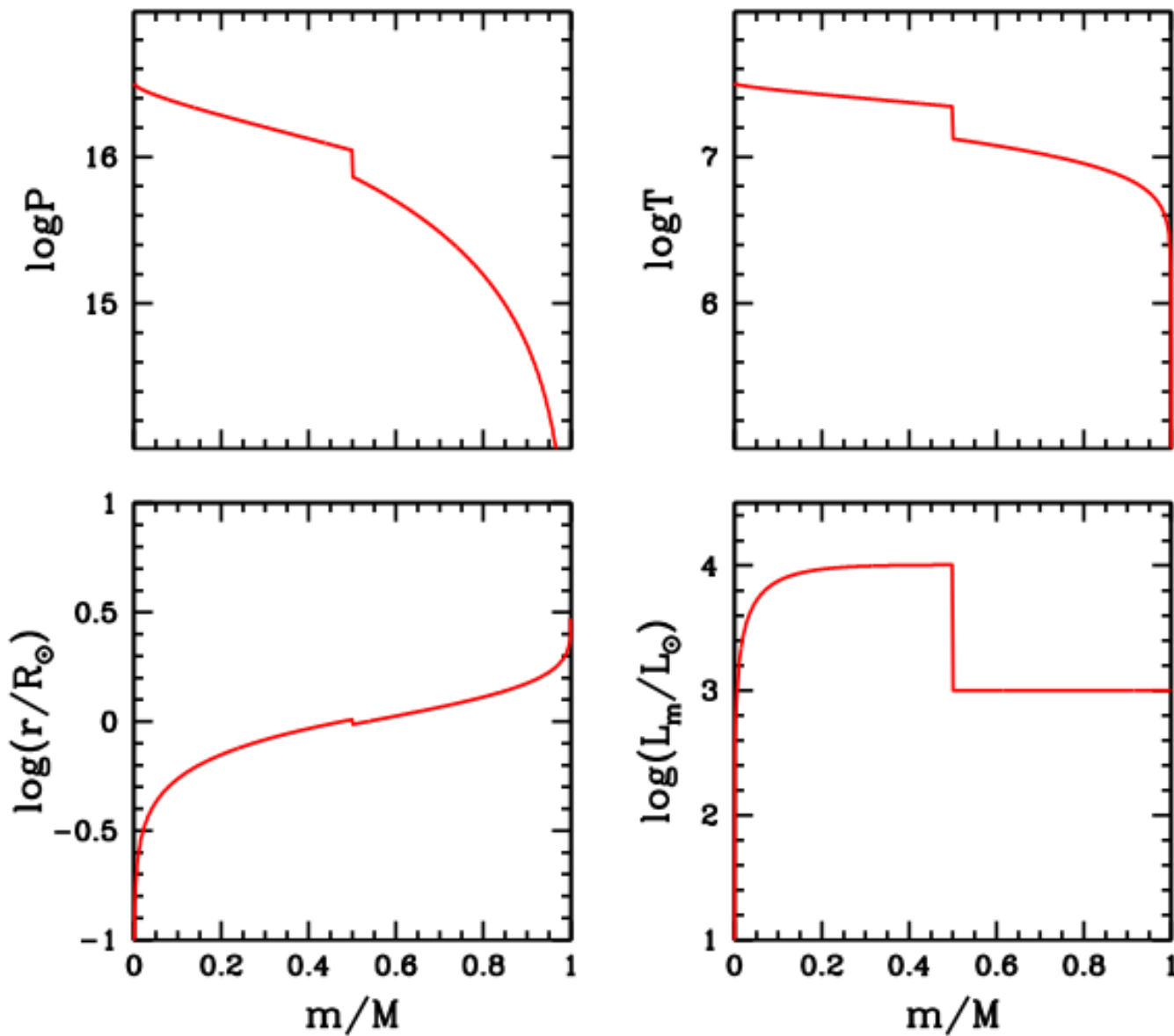
guess

$\log L_m$



guess

Stellar Models



Stellar Models

Boundary Conditions



$\log P_c$



$\log R$



$\log T_c$



$\log L$



$\Delta \log P$

$\Delta \log T$

$\Delta \log r$

$\Delta \log L_m$

Stellar Models

- Repeat using new trial values:

$(\log T_c - d \log T_c)$ and $(\log T_c + d \log T_c)$ with $\log P_c, \log R, \log L$

$(\log P_c - d \log P_c)$ and $(\log P_c + d \log P_c)$ with $\log T_c, \log R, \log L$

$(\log R - d \log R)$ and $(\log R + d \log R)$ with $\log P_c, \log T_c, \log L$

$(\log L - d \log L)$ and $(\log L + d \log L)$ with $\log P_c, \log T_c, \log R$

- Compute new discrepancies in each case.

$$\Delta \log r, \Delta \log P, \Delta \log T, \Delta \log L_m$$

- Get 16 derivatives. e.g.,

$$\frac{\partial(\Delta \log r)}{\partial \log P_c} = \frac{(\Delta \log r)_{\log P_c + d \log P_c} - (\Delta \log r)_{\log P_c - d \log P_c}}{2d \log P_c}$$

Stellar Models

- Use these derivatives to calculate improved boundary conditions.

$$\log P'_c = \log P_c + \delta \log P_c$$

$$\log T'_c = \log T_c + \delta \log T_c$$

$$\log R' = \log R + \delta \log R$$

$$\log L' = \log L + \delta \log L$$

- General idea:

$$-\Delta \log r = \delta \log P_c \frac{\partial(\Delta \log r)}{\partial \log P_c} \rightarrow \delta \log P_c = -\Delta \log r \left[\frac{\partial(\Delta \log r)}{\partial \log P_c} \right]^{-1}$$

- More complicated with 4 variables!

Stellar Models

$$\begin{pmatrix} \frac{\partial(\Delta \log P)}{\partial \log P_c} & \frac{\partial(\Delta \log P)}{\partial \log T_c} & \frac{\partial(\Delta \log P)}{\partial \log R} & \frac{\partial(\Delta \log P)}{\partial \log L} \\ \frac{\partial(\Delta \log T)}{\partial \log P_c} & \frac{\partial(\Delta \log T)}{\partial \log T_c} & \frac{\partial(\Delta \log T)}{\partial \log R} & \frac{\partial(\Delta \log T)}{\partial \log L} \\ \frac{\partial(\Delta \log r)}{\partial \log P_c} & \frac{\partial(\Delta \log r)}{\partial \log T_c} & \frac{\partial(\Delta \log r)}{\partial \log R} & \frac{\partial(\Delta \log r)}{\partial \log L} \\ \frac{\partial(\Delta \log L_m)}{\partial \log P_c} & \frac{\partial(\Delta \log L_m)}{\partial \log T_c} & \frac{\partial(\Delta \log L_m)}{\partial \log R} & \frac{\partial(\Delta \log L_m)}{\partial \log L} \end{pmatrix} \times \begin{pmatrix} \delta \log P_c \\ \delta \log T_c \\ \delta \log R \\ \delta \log L \end{pmatrix} = \begin{pmatrix} -\Delta \log P \\ -\Delta \log T \\ -\Delta \log r \\ -\Delta \log L_m \end{pmatrix}$$

- Invert matrix to solve for
(actually take smaller steps $\sim 0.1x$)

$$\delta \log P_c, \delta \log T_c, \delta \log R, \delta \log L$$

- Iterate until convergence is reached: discrepancies vanish (i.e., drop below a threshold value)